



# **Layered Materials as High Temperature Membranes in Hydrogen Production**

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**Muhammad Sahimi and Theodore Tsotsis**

**Mork Family Department of Chemical Engineering and Materials Science,  
University of Southern California, Los Angeles, CA 90089-1211**



# Outline

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- **Introduction**
- **Membrane synthesis**
- **Membrane characterization**
- **Transport studies**
- **Future work**



# Introduction

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- IGCC plants show promise for environmentally-benign power generation. In these plants coal is gasified to synthesis gas, which is then processed in a water gas-shift reactor (WGSR) to produce  $H_2$  for clean-power generation.
- WGSR is a dual-reactor system, the first reactor (HTS) operating at high temperatures, to attain high reaction rates, followed by a second lower-temperature reactor (LTS), which benefits from increased equilibrium conversions at low temperatures.
- The WGSR exit stream contains  $H_2$ ,  $CO_2$ ,  $H_2O$  and other minor species (e.g.,  $CO$ ). For use in fuel cells (and potentially for  $CO_2$  capture/sequestration),  $CO_2$  is separated using amine absorption or PSA. Both processes are, however, energy- and capital-intensive, and so is the WGSR.



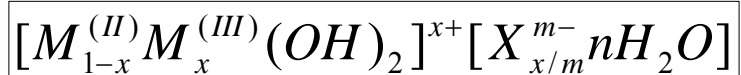
## Introduction, cont.

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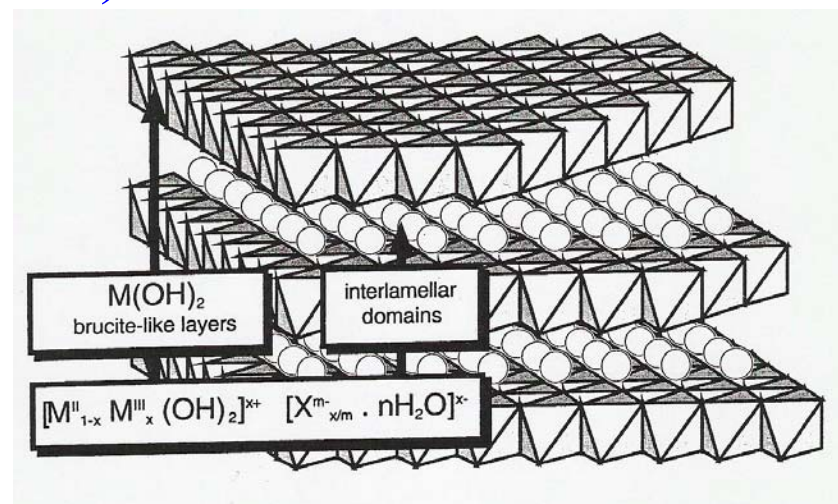
- Our team proposes, instead, a novel membrane reactor (WGSMR), which integrates the WGS and  $H_2$  and/or  $CO_2$  separation steps in a single unit through the use of high temperature membranes.
- The WGSMR has many advantages over the conventional technology. Key to the success of the WGSMR is developing membranes capable of operating in the WGS environment.

# What is a Hydrotalcite?

## LDH (Layered Double Hydroxide)



- M<sup>(II)</sup> :Mg, Mn, Fe, Co, Ni, Cu, Zn, Ga
- M<sup>(III)</sup> :Al, Cr, Mn, Fe, Co, Ni, La
- Anion : m-valence inorganic (CO<sub>3</sub><sup>2-</sup>, OH<sup>-</sup>, NO<sub>3</sub><sup>-</sup>), heteropolyacid, organic anion acid



$$M^{(III)}/M^{(II)}+M^{(III)}$$

$$0.2 \leq x \leq 0.33$$

## ■ Various Applications

catalysts, catalyst supports, ion exchange materials, adsorbents, medical applications



# Membrane Synthesis

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- Two different types of membranes have been prepared: Large area membranes and micromembranes.
- For the large area membranes we utilized as supports macroporous hydrotalcite discs, and alumina tubes and discs.
- For the micromembranes we utilized as supports silicon wafers and perforated stainless steel disks.



## Membrane Synthesis, cont.

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- A number of different techniques have been used for membrane preparation including:
  - Dip-coating using commercial powders and hydrotalcites prepared by our group.
  - Dip-coating using sulfate as a binder
  - Vacuum suction
  - Electrophoretic deposition (EPD)



# Hydrotalcites Used in Membrane Preparation

HT material	Mg/Al ratio from ICP-MS	Synthesis Conditions	
		Mg/Al Molar Ratio	Reaction Conditions.
Sasol Mg50	1.29		
Sasol Mg70	3.0		
Sasol Mg70D	3.0	-	4.6% lactic acid added
Sasol Mg70DS <sup>b</sup>	3.0	-	Ball-milled Sasol Mg70
Aldrich HT	2.19	-	-
USC HT 1	2.89	2.9	Stirring 24 h, at 333K
USC HT 2	3.1	3.0	Stirring 24 h, at 333K

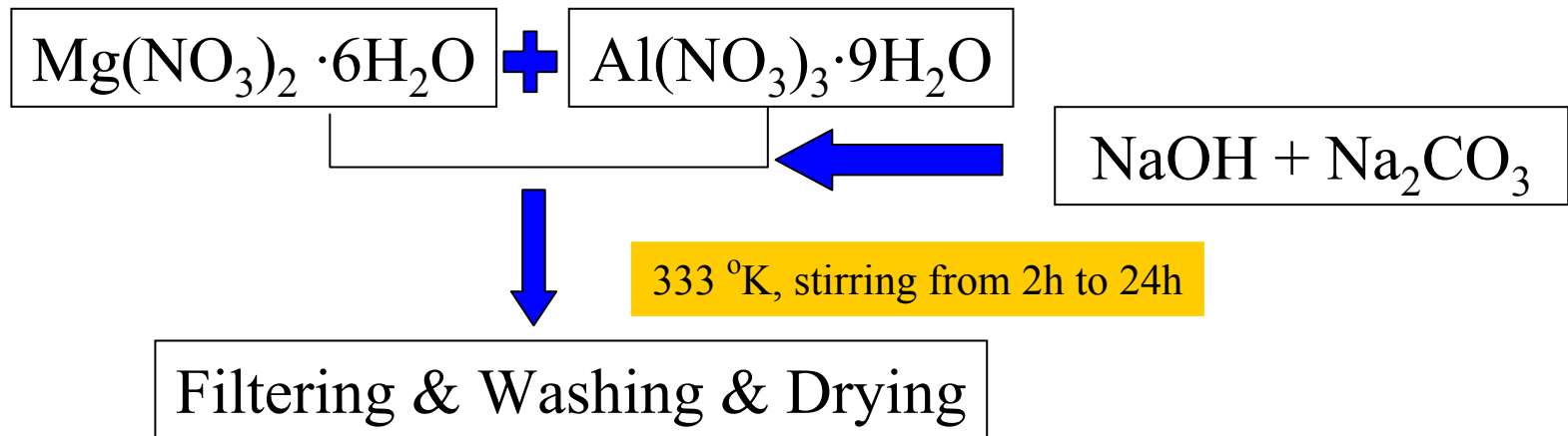




# Hydrotalcite Synthesis

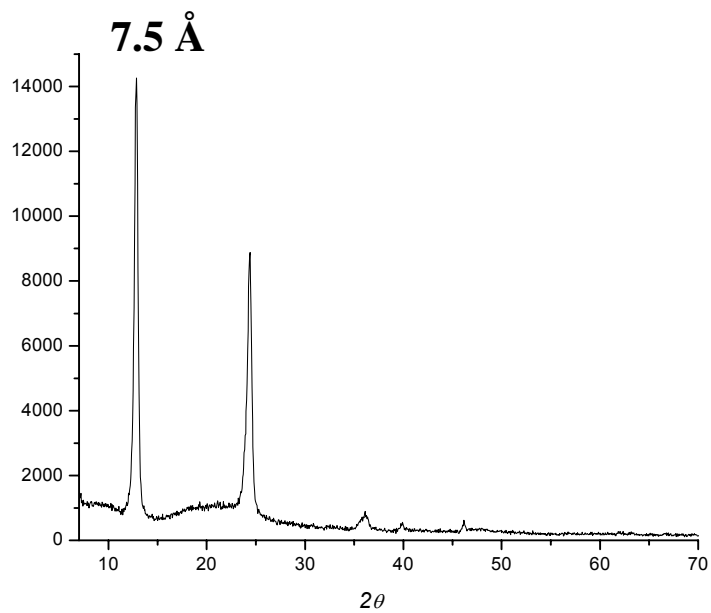
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- We use the co-precipitation method



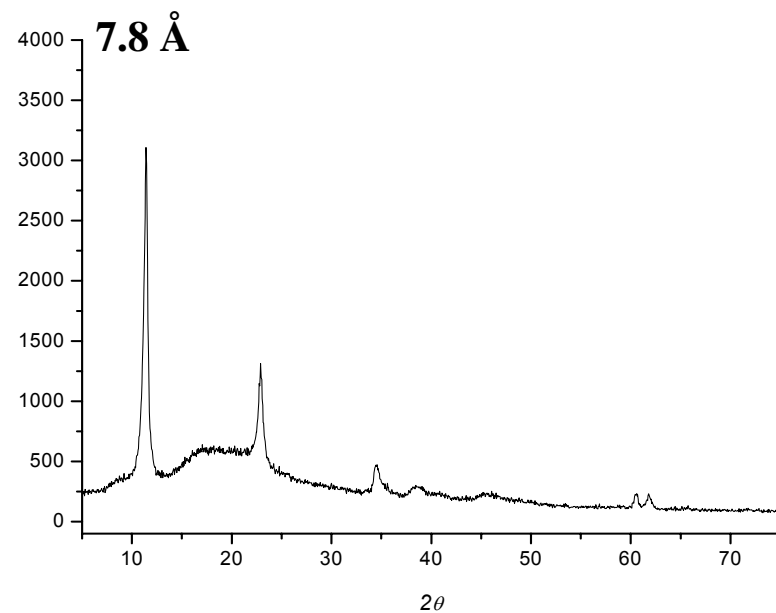
# XRD Spectra

**(003)**



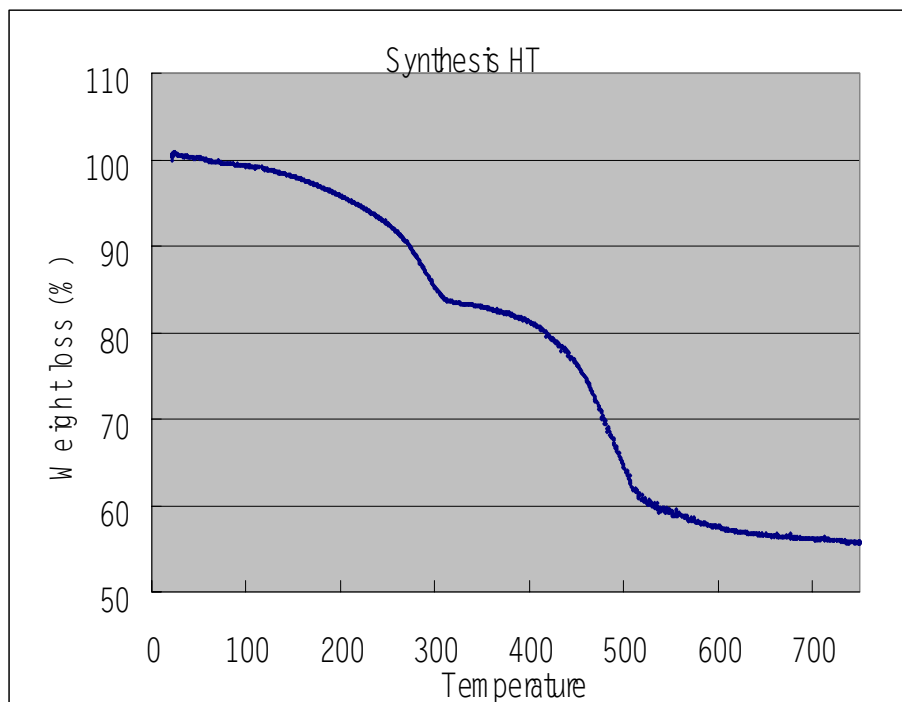
**USC HT**

**(003)**

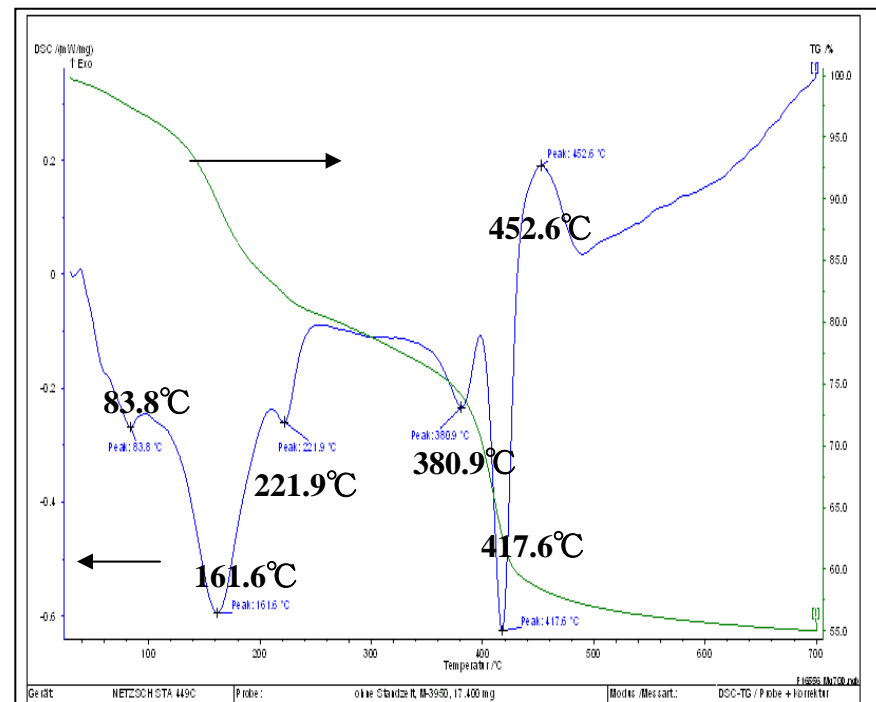


**Mg70D HT**

# TGA Thermograms



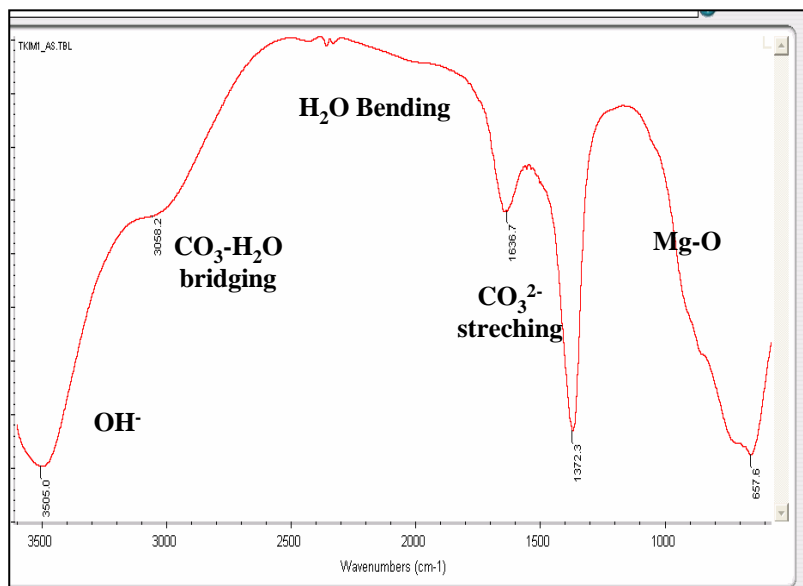
**USC HT**



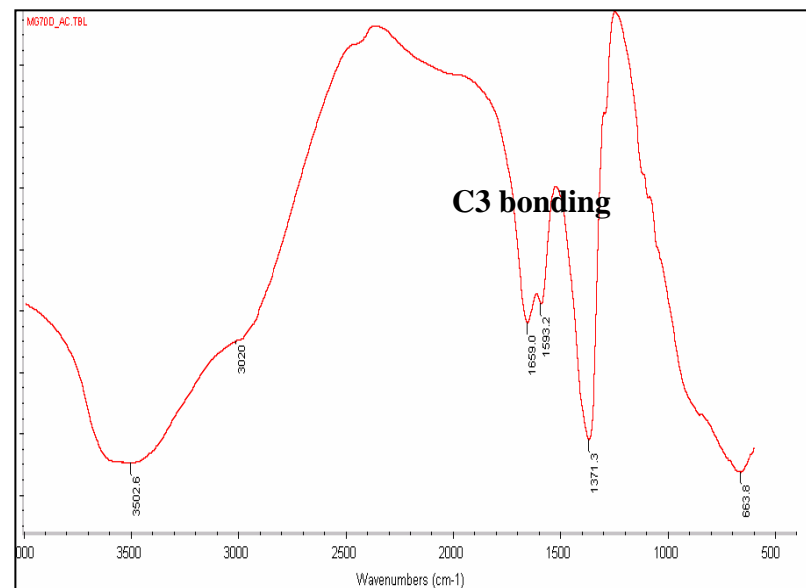
**Mg70D HT**

# FT-IR Spectra

transmission



USC HT

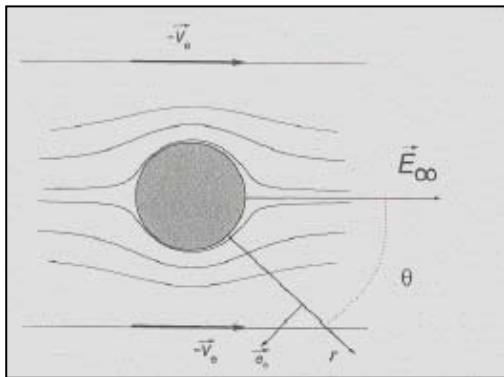


Mg70D HT

# Electrophoretic Deposition (EPD)

Electrophoresis is the process whereby colloids travel through a fluid in response to an applied electric field.

$$M = \int_0^t aAc\mu E . dt$$



$$\mu = \frac{ZEV}{4\pi L \eta}$$

**M=mass deposited in time t**

t = deposition time

a = co-efficient representing the fraction of particles

A = surface area of the electrode

C = particle concentration in the suspension (kg/m<sup>3</sup>)

**μ = electrophoretic mobility (m<sup>2</sup>/Vs)**

E = electric field (V/m)

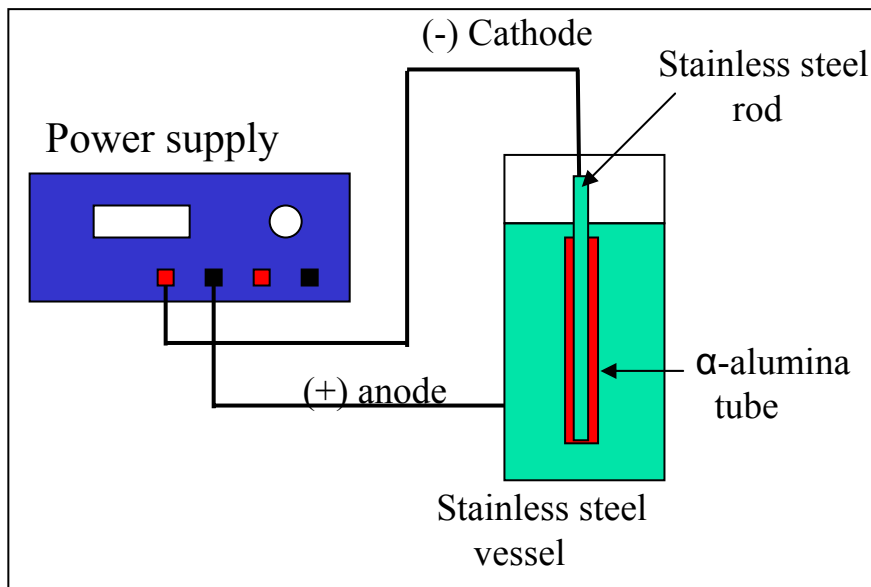
**Z : zeta potential, V : the applied voltage**

E : the dielectric constant of the suspending medium

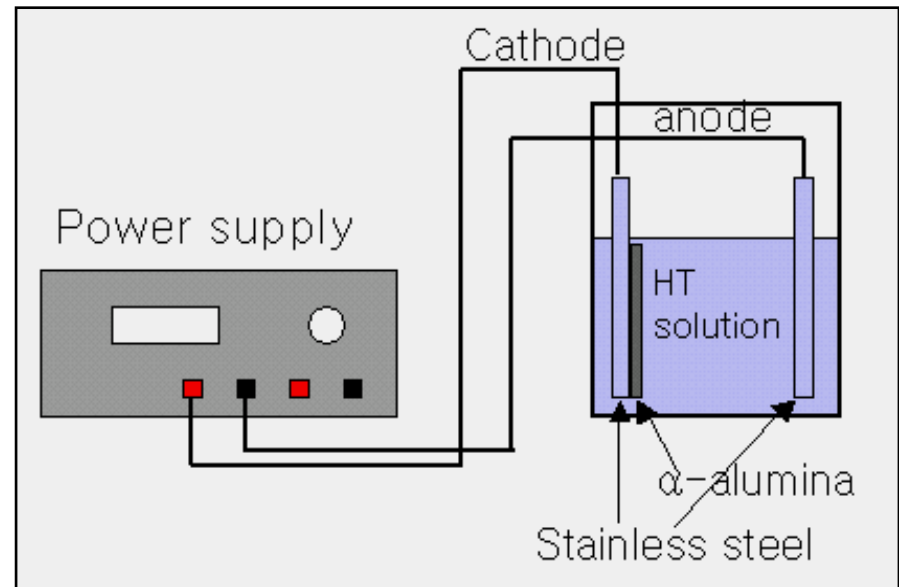
η : the viscosity of the suspension

# Schematic of the EPD System

- **Deposition parameters:** discharge voltage, time, concentration, pH
- **Supports:**  $\alpha$ - alumina (tube, disc), stainless steel porous discs ( $0.2\mu\text{m}$ )
- **HTc used:** Mg 70DS, USC HT



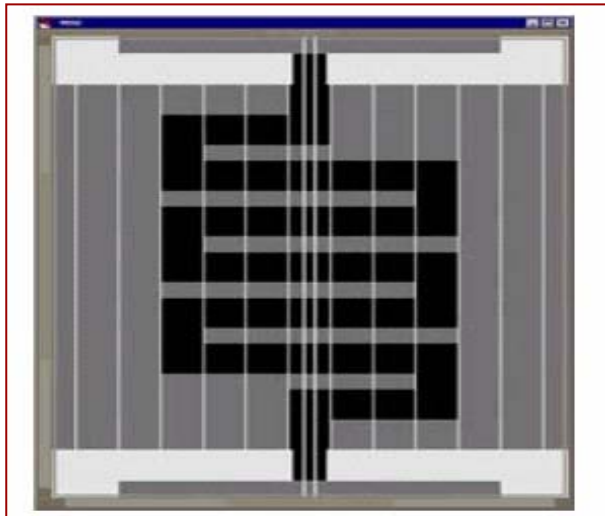
Tube Type



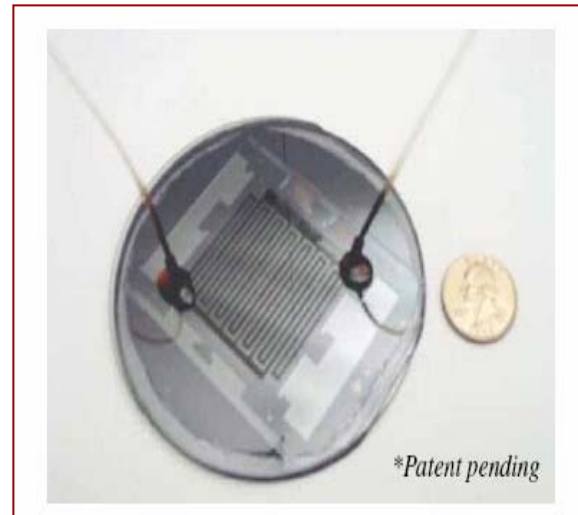
Disc Type

# Micromembranes, Why?

- Easier to prepare crack-free for fundamental investigations
- Potential application in micro fuel-cells and microreactors



Micro Heat Exchanger



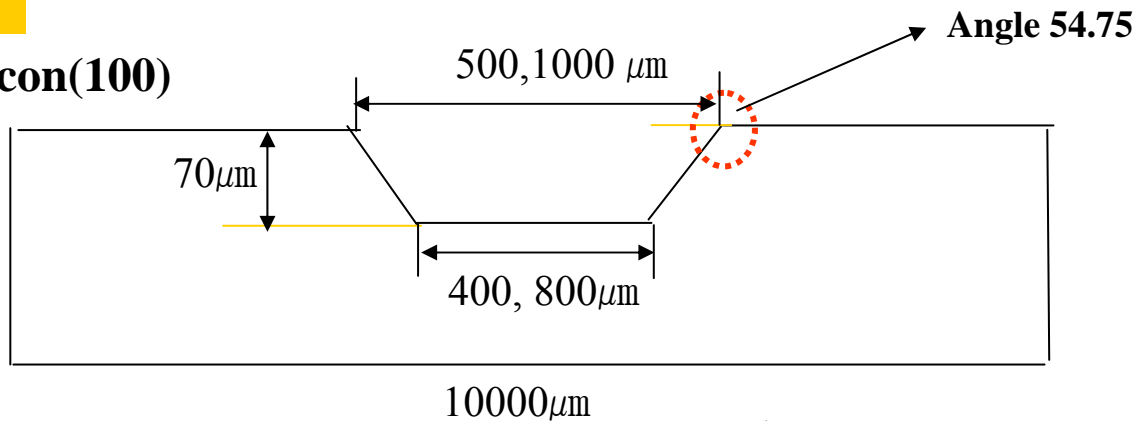
Micro-reactor for Methanol  
Reforming

# Micromembranes, cont.

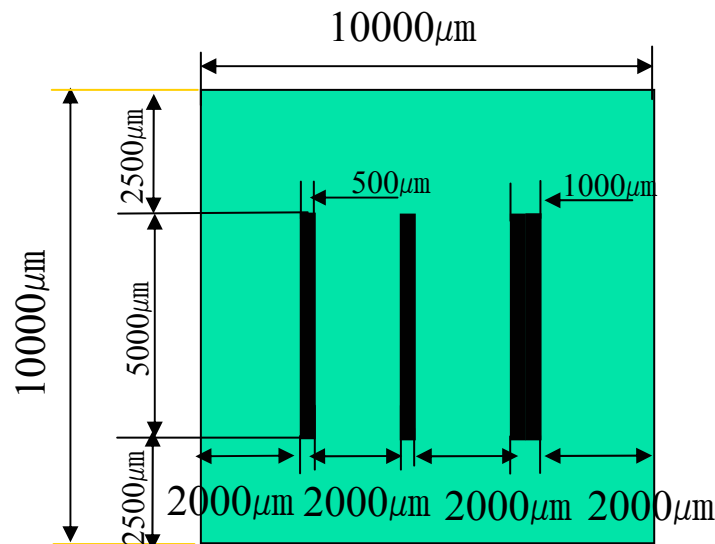
## Silicon-based microchannel membrane

Cross-section

P-Type silicon(100)

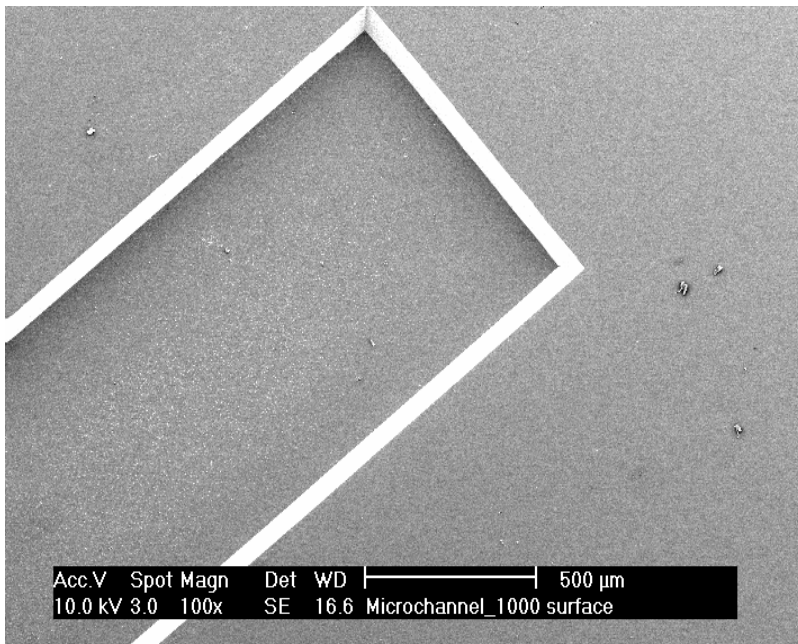


Top surface

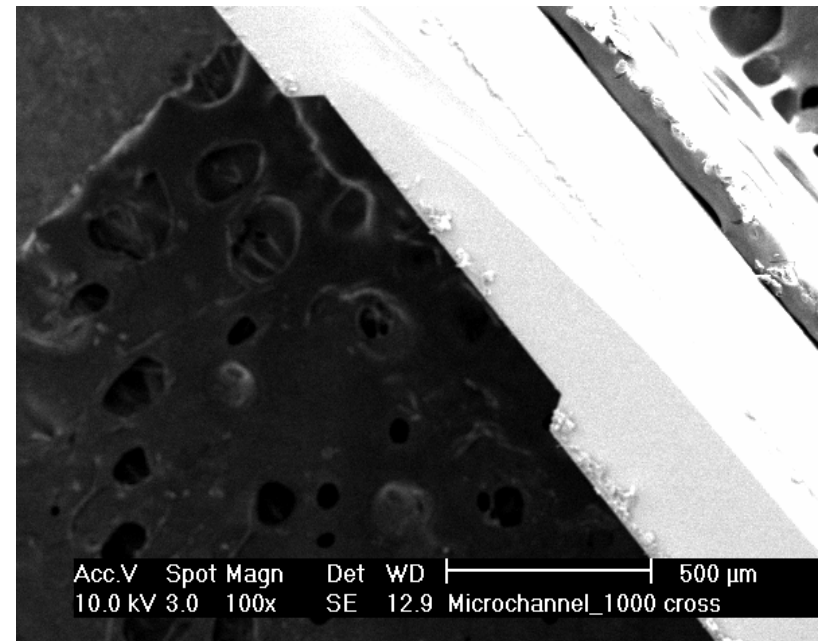




# Micromembranes, cont.



Top view (X100)



Cross-section view (X100)

# Si-Wafer Supported Micromembranes, Fabrication Process

Photolithography step

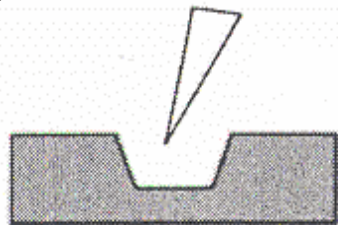


Etching step

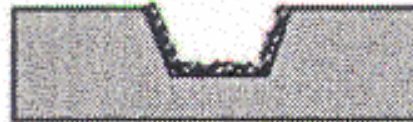


HT Coating/removing  
support silicon layer

No	Intermediate layer	Coating method	Conditions
1	None	Colloidal HT coating drop-wise by a micropipette	Dry at 110°C for 12 h
2		Seed deposition followed by hydrothermal aging	Dry at 110°C for 12 h (after seed deposition) 160 °C for 24 h (hydrothermal aging)
3	$\gamma$ -alumina	Colloidal HT coating drop-wise by a micropipette	Dry at 110°C for 12 h



Adding the HT



Etching  
with KOH

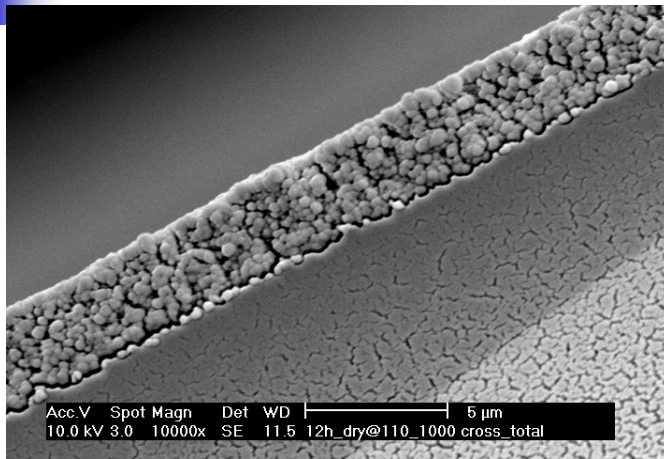


-w/, w/o sublayer  
( $\gamma$ -alumina)

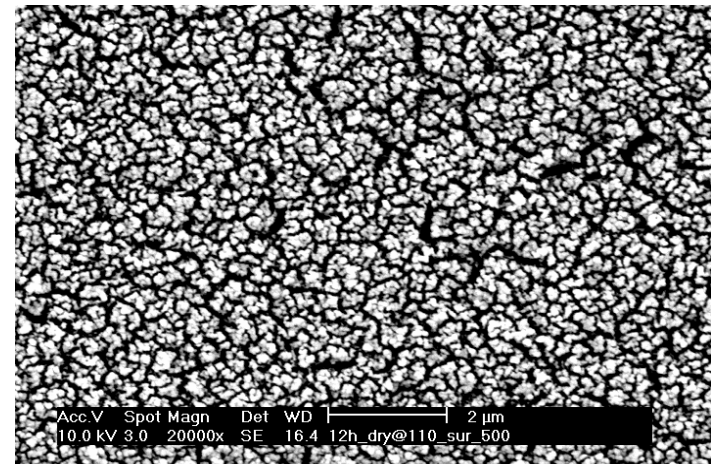
HT coated Si

HT Membrane

# Si Micromembranes, cont.



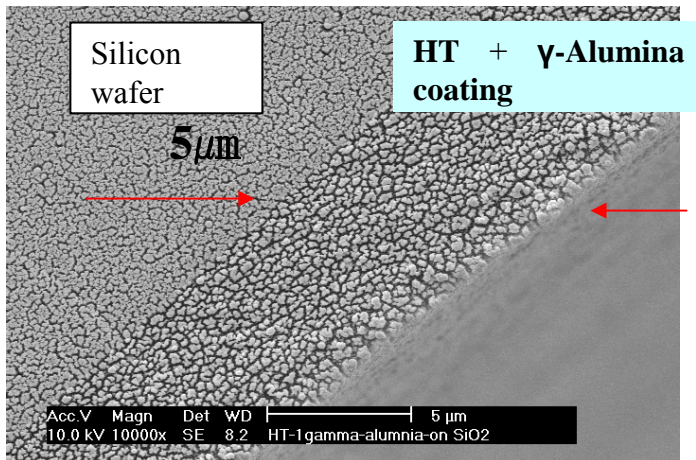
HT membrane on Si, Cross-section



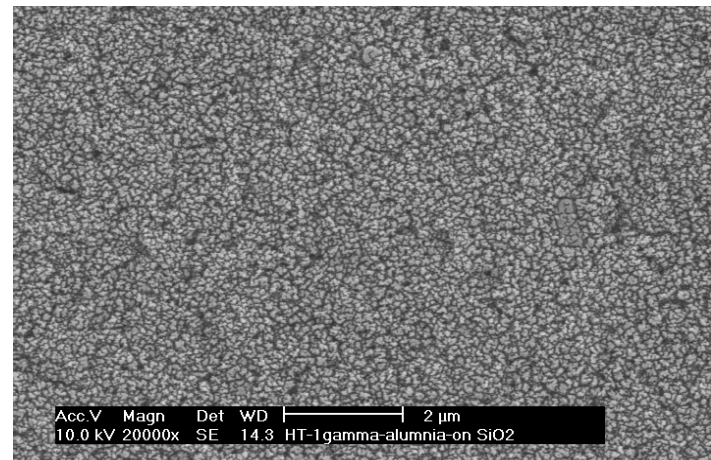
X 1 K

X 2 K

HT membrane on Si, top surface



HT membrane on Si with alumina sublayer, Cross-section



X 10 K

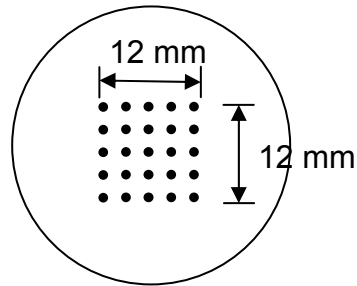
X 20 K

HT membrane on Si with alumina sublayer Surface view)

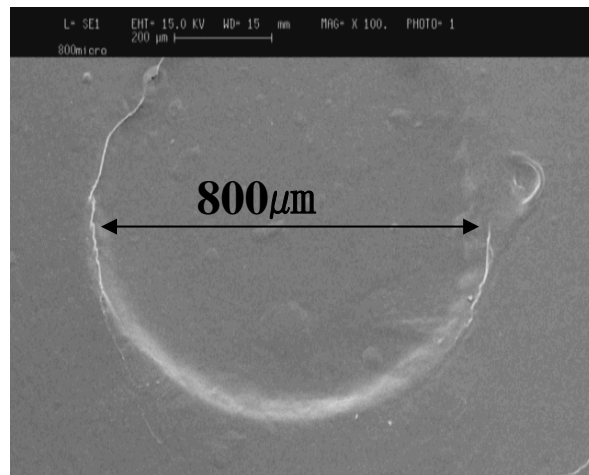


# Stainless Steel Micromembranes

5 X 5 ( Holes' dia. :  $800\mu\text{m}$ )



Stainless steel disc

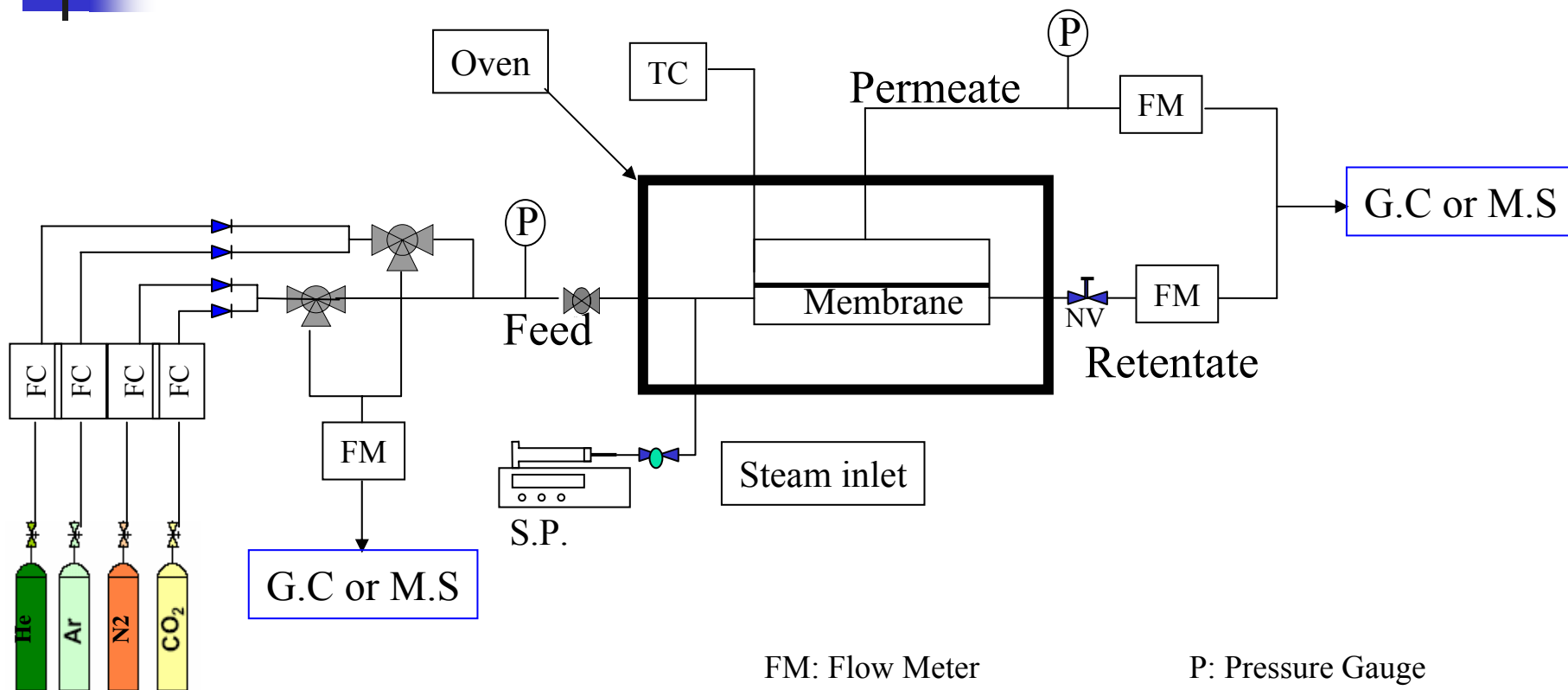


Top surface X100



Top surface X20K

# Permeation Apparatus



FM: Flow Meter

TC: Temperature Controller

FC: Flow Controller (Condyne)

SP: Syringe Pump

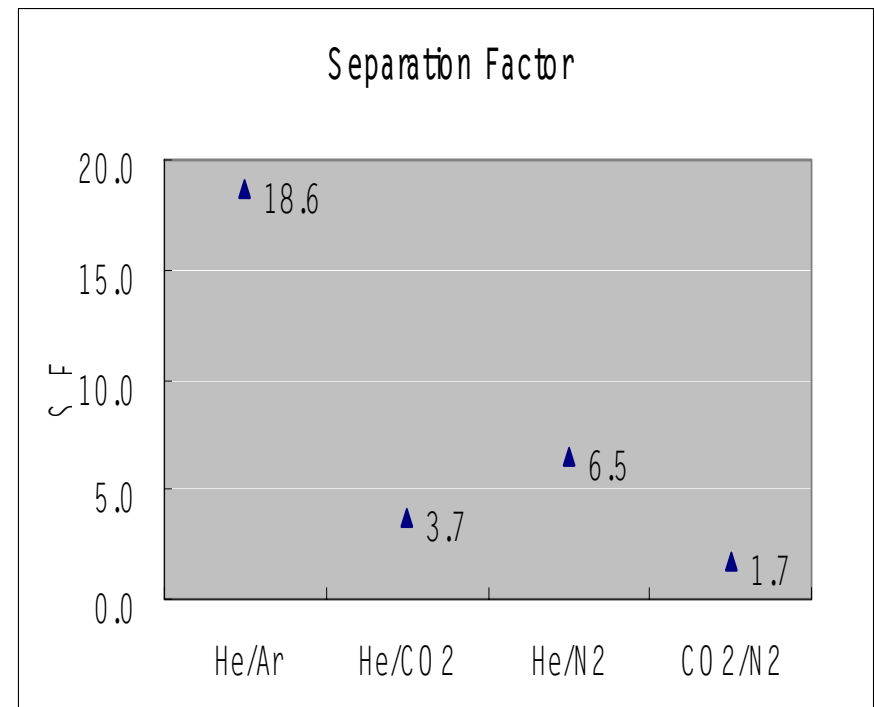
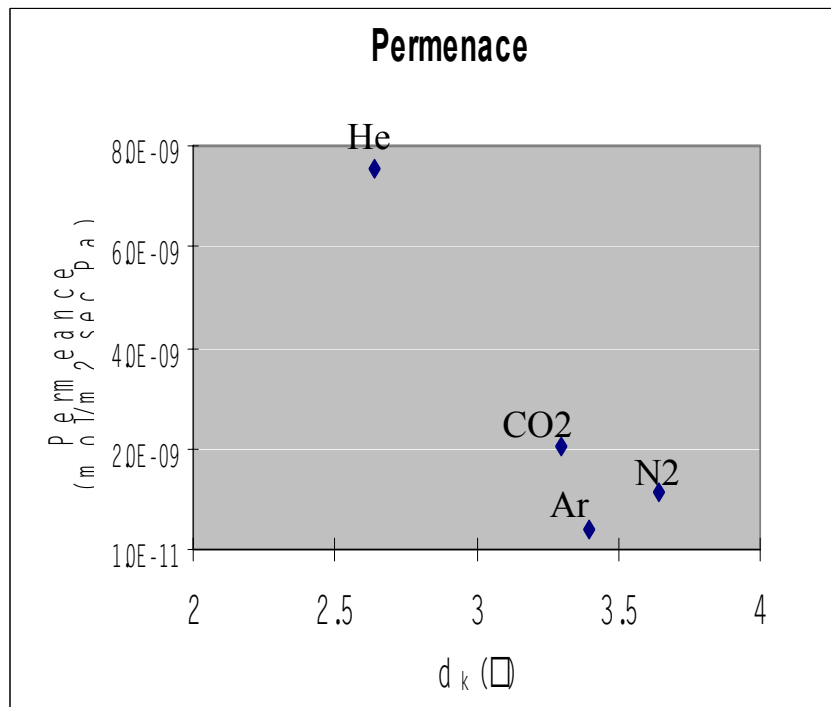
P: Pressure Gauge

NV: Needle Valve

# Micromembranes

$\Delta P = 30$  psi,  $25^\circ\text{C}$

Permenace :  $\text{N}_2 < \text{CO}_2$





## Membranes Prepared with Sulfate Binder

HT source	Coating conditions	Pressure drop (psi)	CO <sub>2</sub>	N <sub>2</sub>	N <sub>2</sub> /CO <sub>2</sub>
Mg50	Dip-coating, 3 layers	30	2.65E-08	3.37E-08	1.27
		40	3.11E-08	3.38E-08	1.09
	In-situ 30min	30	1.60E-07	1.46E-07	0.91
		40	1.82E-07	1.65E-07	0.90
	In-situ 3 h	30	3.43E-07	3.07E-07	0.90
		40	3.96E-07	3.56E-07	0.90
Mg70D	Dip-coating, 1 layer	30	1.54E-06	1.72E-06	1.12
	Dip-coating, 3 layers	30	5.63E-07	6.93E-07	1.23



# EPD Membranes

Name	Support	EPD conditions				N <sub>2</sub> Permeance (mol/m <sup>2</sup> sPa)		N <sub>2</sub> /CO <sub>2</sub>	
		voltage /coating times	Time	pH	Solution	$\Delta P$		$\Delta P$	
						30 psi	40 psi	30 psi	40 psi
E1	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> Tube	1V/1	24 h	12	Synth. HT	$1.5 \times 10^{-7}$	$1.6 \times 10^{-7}$	1.16	1.05
E2	$\gamma$ -Al <sub>2</sub> O <sub>3</sub> Tube	2V/4	24h	12	Synth. HT	$2.7 \times 10^{-7}$	$2.9 \times 10^{-7}$	1.13	1.17
E3	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> disc	2V/3	24h	12	Synth. HT	$2.6 \times 10^{-7}$	$3.0 \times 10^{-7}$	1.13	1.03
E4	S-5 <sup>a</sup>	1V/1	1 h	7	Mg70DS <sup>b</sup>	$2.1 \times 10^{-7}$	-	1.28	-
E5	HT disc	1V/1	3h	7	Mg70DS <sup>b</sup>	$6.6 \times 10^{-7}$	$7.0 \times 10^{-7}$	1.33	1.29
E6	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> Tube	1V/1	1.5h	7	Mg70DS <sup>b</sup>	$5.4 \times 10^{-7}$	-	0.83	-
E7	S-5 <sup>c</sup>	20V/3	1h	7	Mg70DS <sup>b</sup>	$2.7 \times 10^{-7}$	$3.8 \times 10^{-7}$	0.75	0.88
E8	S-5 <sup>c</sup>	20V/2	1h	7	Mg70DS <sup>b</sup>	$2.0 \times 10^{-7}$	-	0.86	-



# Membranes Prepared by Vacuum Suction

Gas (MW))	Permeance $\times 10^{-8}$ (mol/m <sup>2</sup> s Pa)		Permselectivity					
			He/gas			N <sub>2</sub> /gas		
	30 psi	40 psi	Ideal Knudsen value	Experimental Result		Ideal Knudse n value	Experimenta l Result	
				30 psi	40 psi		30 psi	40 psi
He (4)	5.78	5.38	1.0	1.0	1.0	0.38	0.22	0.25
N <sub>2</sub> (28)	1.28	1.36	2.65	4.52	3.96	1.0	1.0	1.0
Ar (40)	0.95	0.96	3.16	6.08	5.60	1.20	1.35	1.42
CO <sub>2</sub> (44)	0.67	0.66	3.32	8.63	8.15	1.25	1.91	2.06



# Membranes Prepared by Vacuum Suction, cont

Temp. (°C)	Permeance $\times 10^{-8}$ (mol/m <sup>2</sup> s Pa)				Permselectivity				
	He	N <sub>2</sub>	Ar	CO <sub>2</sub>	He/CO <sub>2</sub>	He/Ar	He/N <sub>2</sub>	N <sub>2</sub> /CO <sub>2</sub>	N <sub>2</sub> /Ar
25	9.04	1.96	1.49	1.08	8.35	6.09	4.61	1.81	1.32
80	6.62	1.81	0.67	1.10	6.02	9.94	3.66	1.64	2.71
150	4.78	1.08	0.85	0.71	6.78	5.63	4.41	1.54	1.28



# Mixed-gas Permeation Tests

Membrane	Number of Coatings	Separation Factor(N <sub>2</sub> /CO <sub>2</sub> )	
		Single gas	Gas Mixture
Dipcoating <sup>a</sup> by 1.25 wt% Mg70D solution	4	1.3	1.4
Dipcoating <sup>a</sup> by 5wt% Mg70D solution	2	1.27	1.4
EPD E#6 <sup>b</sup>	EPD 1 <sup>st</sup> coating	0.83	0.72

$\Delta P=30\text{psi}$ , R.T., Feed gas N<sub>2</sub>:CO<sub>2</sub> = 0.4:0.6,  
<sup>a</sup>:  $\alpha$ -alumina tube, <sup>b</sup>: Feed gas N<sub>2</sub>:CO<sub>2</sub> =0.7:0.3



# Mixed-gas Permeation Tests

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Temp.(K)	Permeance $\times 10^{-7}$ (mol/m <sup>2</sup> sPa)		Separation Factor (CO <sub>2</sub> /N <sub>2</sub> )
	CO <sub>2</sub>	N <sub>2</sub>	
298 K	4.38	3.15	1.39
423 K	4.69	2.86	1.64
473 K	5.05	2.49	2.03

$\Delta P = 30$  psi, Feed gas N<sub>2</sub>:CO<sub>2</sub>=0.7:0.3



## Conclusions

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- A number of techniques have been developed and studied for the preparation of HT membranes.
- Different membranes have been developed and tested for their permeation characteristics towards single gases and mixtures of gases.
- A number of these membranes were shown to be nanoporous, and some of them show permselectivity towards CO<sub>2</sub>.



## Acknowledgement

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